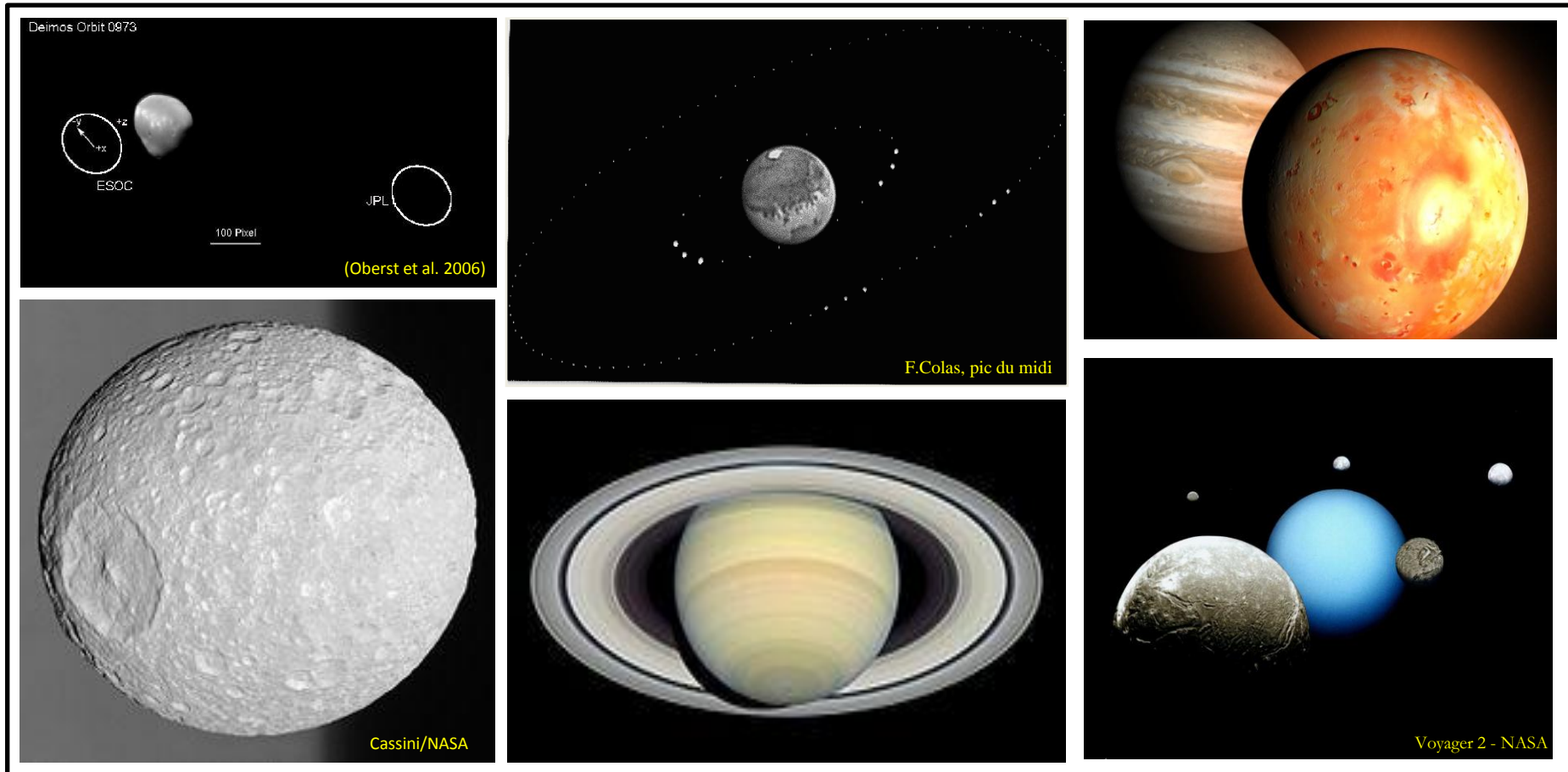


Orbit determination of natural satellites

V. Lainey (IMCCE-Paris Observatory)



Outline:

- 1- Comparison between spacecraft and natural satellite orbitography
- 2- Example of the Mars system
- 3- The ESPaCE network (FP7)

1- Comparison between spacecraft and natural satellite orbitography

1- Comparison between spacecraft and natural satellite orbitography

→ *We follow exactly the same methodology...*

Method in three steps:

- 1- modeling of the dynamical system
- 2- gathering the observations
- 3- fitting the model to the observations

Today, this kind of work is done completely numerically

S/C: GINS, DPODP, GEODYN, ...

SAT: NOE, ...

1- Comparison between spacecraft and natural satellite orbitography

Step 1: Modeling of the dynamical system

Equations of motion

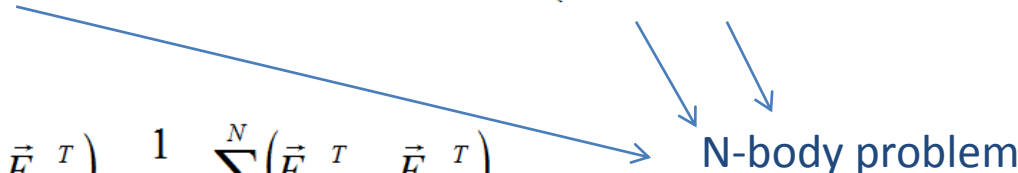
$$\ddot{\vec{r}}_i = -G(m_0 + m_i) \left(\frac{\vec{r}_i}{r_i^3} - \nabla_i U_{\vec{r}_i \hat{0}} + \nabla_0 U_{\vec{r}_i \hat{0}} \right) + \sum_{j=1, j \neq i}^N Gm_j \left(\frac{\vec{r}_j - \vec{r}_i}{r_{ij}^3} - \frac{\vec{r}_j}{r_j^3} - \nabla_j U_{\vec{r}_j \hat{i}} + \nabla_i U_{\vec{r}_j \hat{i}} + \nabla_j U_{\vec{r}_j \hat{0}} - \nabla_0 U_{\vec{r}_j \hat{0}} \right)$$
$$+ \frac{(m_0 + m_i)}{m_i m_0} \left(\vec{F}_{\vec{r}_i \hat{0}}^T - \vec{F}_{\vec{r}_i \hat{0}}^T \right) - \frac{1}{m_0} \sum_{j=1, j \neq i}^N \left(\vec{F}_{\vec{r}_j \hat{0}}^T - \vec{F}_{\vec{r}_j \hat{0}}^T \right)$$

1- Comparison between spacecraft and natural satellite orbitography

Step 1: Modeling of the dynamical system

Equations of motion

$$\ddot{\vec{r}}_i = -G(m_0 + m_i) \left(\frac{\vec{r}_i}{r_i^3} - \nabla_i U_{\vec{r}_i \hat{0}} + \nabla_0 U_{\vec{r}_i \hat{0}} \right) + \sum_{j=1, j \neq i}^N Gm_j \left(\frac{\vec{r}_j - \vec{r}_i}{r_{ij}^3} - \frac{\vec{r}_j}{r_j^3} - \nabla_j U_{\vec{r}_j \hat{i}} + \nabla_i U_{\vec{r}_j \hat{i}} + \nabla_j U_{\vec{r}_j \hat{0}} - \nabla_0 U_{\vec{r}_j \hat{0}} \right)$$

The diagram shows three blue arrows originating from the equation above. One arrow points from the first term of the equation to the text 'N-body problem'. Two other arrows point from the second term of the equation to the same text.

$$+ \frac{(m_0 + m_i)}{m_i m_0} (\vec{F}_{\vec{r}_i \hat{0}}^T - \vec{F}_{\vec{r}_i \hat{0}}^T) - \frac{1}{m_0} \sum_{j=1, j \neq i}^N (\vec{F}_{\vec{r}_j \hat{0}}^T - \vec{F}_{\vec{r}_j \hat{0}}^T)$$

N-body problem

1- Comparison between spacecraft and natural satellite orbitography

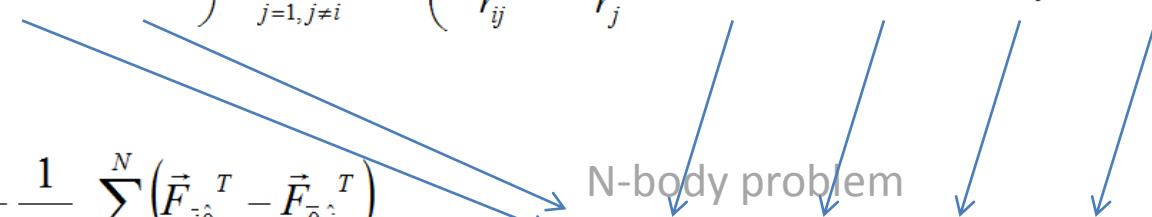
Step 1: Modeling of the dynamical system

Equations of motion

$$\ddot{\vec{r}}_i = -G(m_0 + m_i) \left(\frac{\vec{r}_i}{r_i^3} - \nabla_i U_{\vec{r}_i \hat{0}} + \nabla_0 U_{\vec{r}_i \hat{0}} \right) + \sum_{j=1, j \neq i}^N Gm_j \left(\frac{\vec{r}_j - \vec{r}_i}{r_{ij}^3} - \frac{\vec{r}_j}{r_j^3} - \nabla_j U_{\vec{r}_j \hat{i}} + \nabla_i U_{\vec{r}_j \hat{i}} + \nabla_j U_{\vec{r}_j \hat{0}} - \nabla_0 U_{\vec{r}_j \hat{0}} \right)$$

$+$ $\frac{(m_0 + m_i)}{m_i m_0} (\vec{F}_{\vec{r}_i \hat{0}}^T - \vec{F}_{\vec{r}_i \hat{0}}^T) - \frac{1}{m_0} \sum_{j=1, j \neq i}^N (\vec{F}_{\vec{r}_j \hat{0}}^T - \vec{F}_{\vec{r}_j \hat{0}}^T)$

N-body problem
Extended gravity fields



1- Comparison between spacecraft and natural satellite orbitography

Step 1: Modeling of the dynamical system

Equations of motion

$$\ddot{\vec{r}}_i = -G(m_0 + m_i) \left(\frac{\vec{r}_i}{r_i^3} - \nabla_i U_{\vec{r}_i \hat{0}} + \nabla_0 U_{\vec{r}_i \hat{0}} \right) + \sum_{j=1, j \neq i}^N Gm_j \left(\frac{\vec{r}_j - \vec{r}_i}{r_{ij}^3} - \frac{\vec{r}_j}{r_j^3} - \nabla_j U_{\vec{r}_j \hat{i}} + \nabla_i U_{\vec{r}_j \hat{i}} + \nabla_j U_{\vec{r}_j \hat{0}} - \nabla_0 U_{\vec{r}_j \hat{0}} \right)$$

$$+ \frac{(m_0 + m_i)}{m_i m_0} (\vec{F}_{\vec{r}_i \hat{0}}^T - \vec{F}_{\vec{r}_i \hat{0}}^T) - \frac{1}{m_0} \sum_{j=1, j \neq i}^N (\vec{F}_{\vec{r}_j \hat{0}}^T - \vec{F}_{\vec{r}_j \hat{0}}^T)$$

N-body problem
Extended gravity fields
Tidal effects

1- Comparison between spacecraft and natural satellite orbitography

Step 1: Modeling of the dynamical system

Equations of motion

$$\ddot{\vec{r}}_i = -G(m_0 + m_i) \left(\frac{\vec{r}_i}{r_i^3} - \nabla_i U_{\vec{r}_i \hat{0}} + \nabla_0 U_{\vec{r}_i \hat{0}} \right) + \sum_{j=1, j \neq i}^N Gm_j \left(\frac{\vec{r}_j - \vec{r}_i}{r_{ij}^3} - \frac{\vec{r}_j}{r_j^3} - \nabla_j U_{\vec{r}_j \hat{i}} + \nabla_i U_{\vec{r}_j \hat{i}} + \nabla_j U_{\vec{r}_j \hat{0}} - \nabla_0 U_{\vec{r}_j \hat{0}} \right)$$

$$+ \frac{(m_0 + m_i)}{m_i m_0} \left(\vec{F}_{\vec{r}_i \hat{0}}^T - \vec{F}_{\vec{r}_i \hat{0}}^T \right) - \frac{1}{m_0} \sum_{j=1, j \neq i}^N \left(\vec{F}_{\vec{r}_j \hat{0}}^T - \vec{F}_{\vec{r}_j \hat{0}}^T \right)$$

N-body problem

Extended gravity fields

Tidal effects

+ Few relativistic terms

1- Comparison between spacecraft and natural satellite orbitography

Step 1: Modeling of the dynamical system

Equations of motion

$$\ddot{\vec{r}}_i = -G(m_0 + m_i) \left(\frac{\vec{r}_i}{r_i^3} - \nabla_i U_{\vec{r}_i \hat{0}} + \nabla_0 U_{\vec{r}_i \hat{0}} \right) + \sum_{j=1, j \neq i}^N Gm_j \left(\frac{\vec{r}_j - \vec{r}_i}{r_{ij}^3} - \frac{\vec{r}_j}{r_j^3} - \nabla_j U_{\vec{r}_j \hat{i}} + \nabla_i U_{\vec{r}_j \hat{i}} + \nabla_j U_{\vec{r}_j \hat{0}} - \nabla_0 U_{\vec{r}_j \hat{0}} \right)$$

$$+ \frac{(m_0 + m_i)}{m_i m_0} \left(\vec{F}_{\vec{r}_i \hat{0}}^T - \vec{F}_{\vec{r}_i \hat{0}}^T \right) - \frac{1}{m_0} \sum_{j=1, j \neq i}^N \left(\vec{F}_{\vec{r}_j \hat{0}}^T - \vec{F}_{\vec{r}_j \hat{0}}^T \right)$$

N-body problem
Extended gravity fields
Tidal effects
+ Few relativistic terms

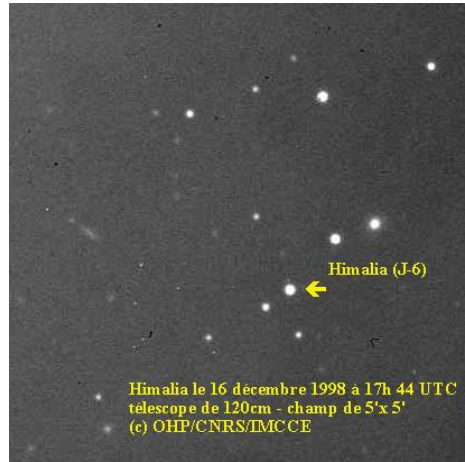
Variational equations

$$\frac{\partial}{\partial c_l} \left(\frac{d^2 \vec{r}_i}{dt^2} \right) = \frac{1}{m_i} \left[\sum_j \left(\frac{\partial \vec{F}_i}{\partial \vec{r}_j} \frac{\partial \vec{r}_j}{\partial c_l} + \frac{\partial \vec{F}_i}{\partial \dot{\vec{r}}_j} \frac{\partial \dot{\vec{r}}_j}{\partial c_l} \right) + \frac{\partial \vec{F}_i}{\partial c_l} \right]$$

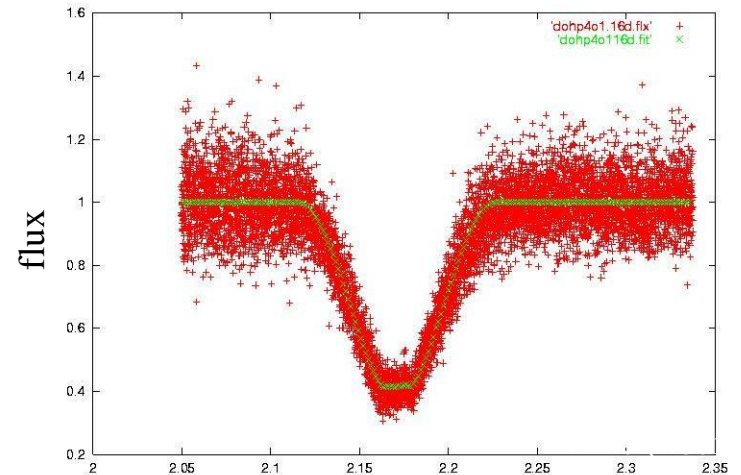
1- Comparison between spacecraft and natural satellite orbitography

Step 2: gathering the observations

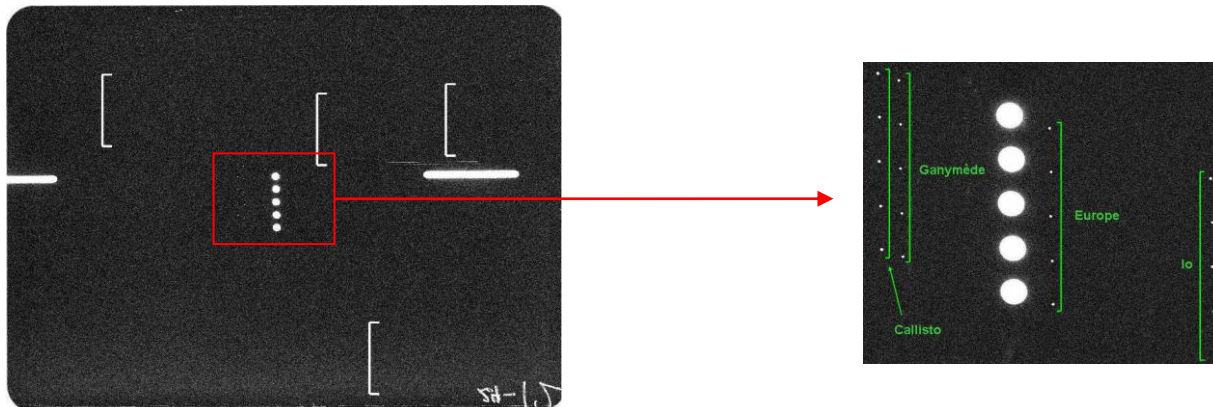
Direct astrometric measurement



Undirect astrometric measurement (photometry)



Astrometric remeasurement (benefit from modern scanning machine)



1- Comparison between spacecraft and natural satellite orbitography

Step 3: Fitting the model to the observations

Step 2 (**observations**)

Step 1 (Integration of the equations of motion + variational equations)

Step 3 (fitting the model)
Approximation by a linear system
=> *least squares method*

$$\begin{pmatrix} O - C \end{pmatrix} = \sum_{l=1}^N A_l(c_l) \cdot \Delta c_l + O((\Delta c_l)^2)$$

unknown

1- Comparison between spacecraft and natural satellite orbitography

Two important points:

1 - S/C have polar orbit while SAT have equatorial orbits

→ SAT and S/C are sensitive to different harmonics of the primary's gravity field

2 - S/C data are regularly splitted into arcs (wheel off loading, drag pressure...) while SAT= 1 arc

→ S/C will be useful for short term dynamics (gravity fields, mutual perturbations...) while SAT will be useful for long term dynamics (tidal effects...)

SAT and S/C dynamics are complementary!!

2- Example of the Mars system

2- Example of the Mars system

Former works:

Sinclair, 1972

Shor, 1975

Sinclair, 1989

Jacobson et al. 1989

Chapront-Touzé, 1990

Morley, 1990

Emelianov et al. 1993

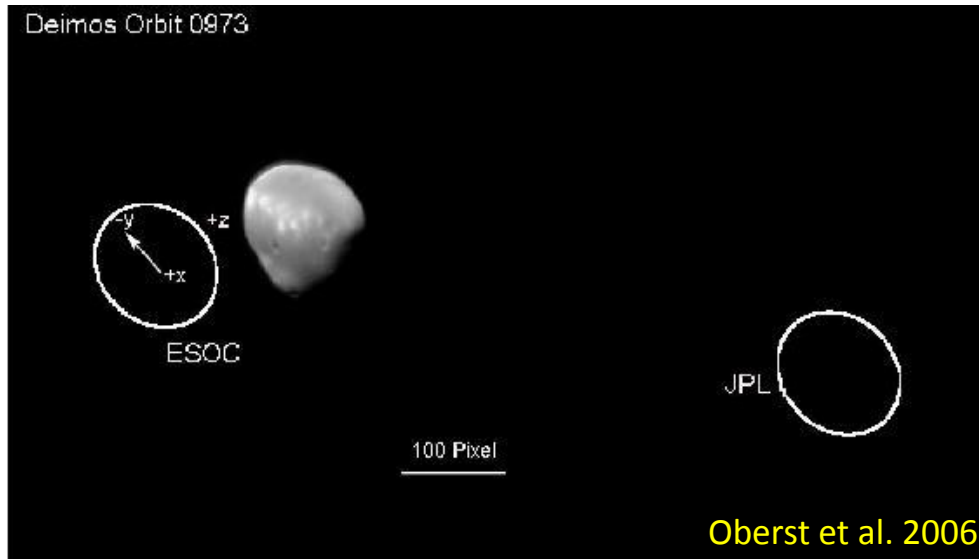


→All these models were analytic

→Tidal effects modelled by a t^2 term in the longitude.

2- Example of the Mars system

Since the 90s the Martian moon ephemerides had drifted...



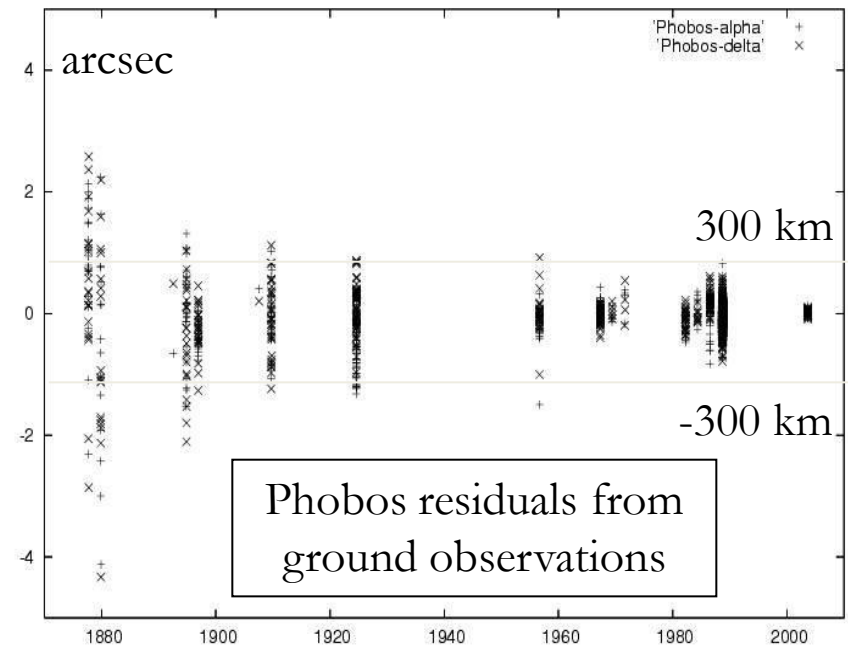
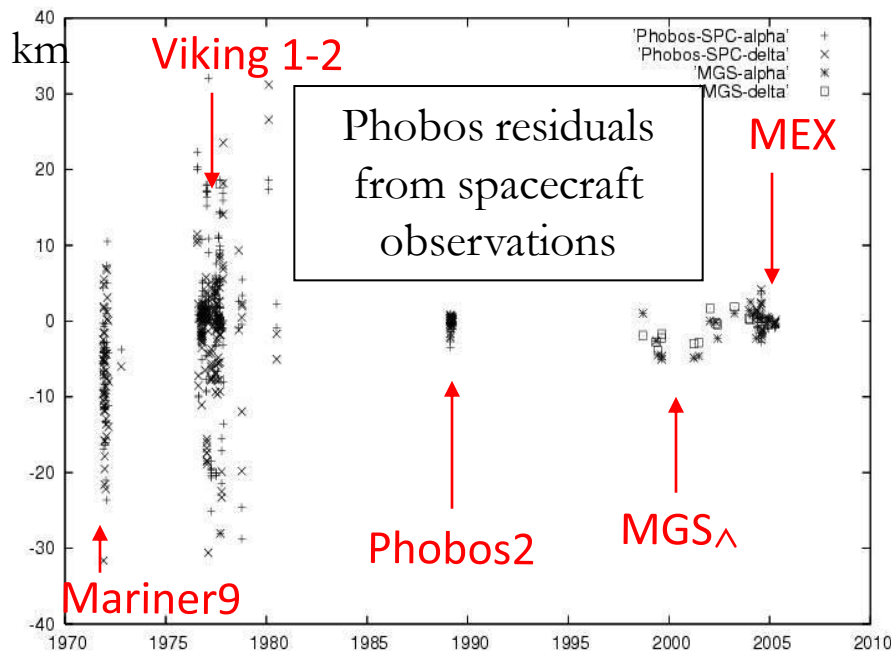
New ephemerides have been developed at JPL and IMCCE/ROB these last years to guarantee a good accuracy of martian moon position in the context of MEX and MRO.

(both ephemerides are based on numerical integration)

See Lainey et al. (2007); Jacobson (2010)

2- Example of the Mars system

Astrometric post-fit residuals for Phobos et Deimos after fit of initial state vectors, Mars dissipation factor Q and Phobos' oblate parameters c_{20} , c_{22} .



Lainey, Dehant and Pätzold (2007)

NB: Just one « arc » was used!!

2- Example of the Mars system

Two current challenges concerning the astrometry of Mars moons:

(precision of measurements=500 metres; more than 30,000 revolutions over 30 years)

1- Influence of Phobos' J_2+6C_{22}
(several kilometres)

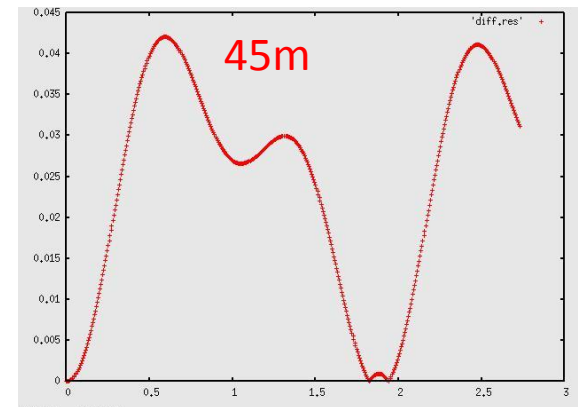
Jacobson (2010) solution in agreement with Willner (2010)

→ Suggests that Phobos is almost homogeneous



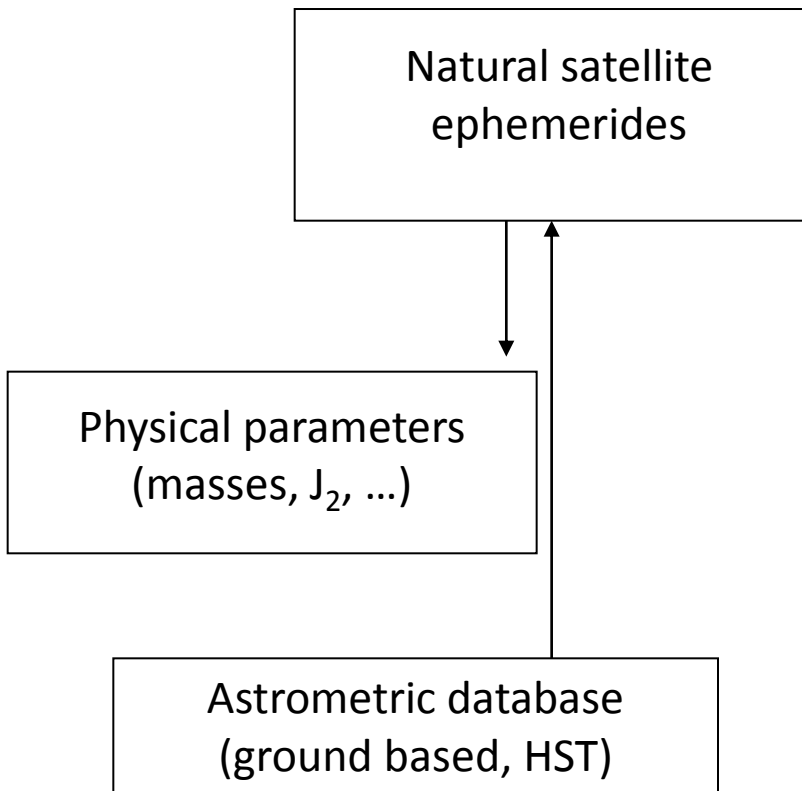
2- Seasonal variations of Mars J_2

→ Signal close to the limit of current accuracy...

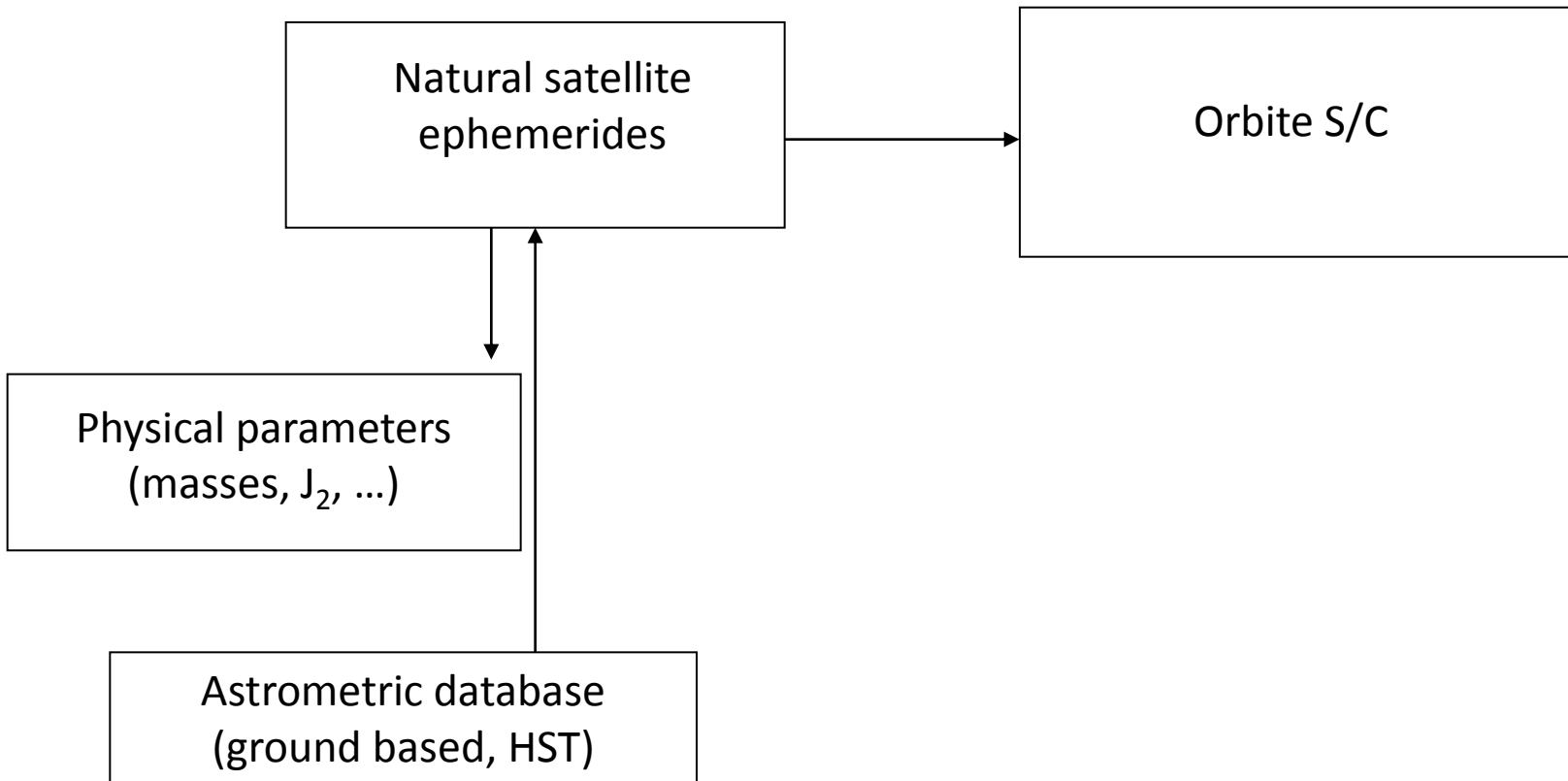


3- The ESPaCE network

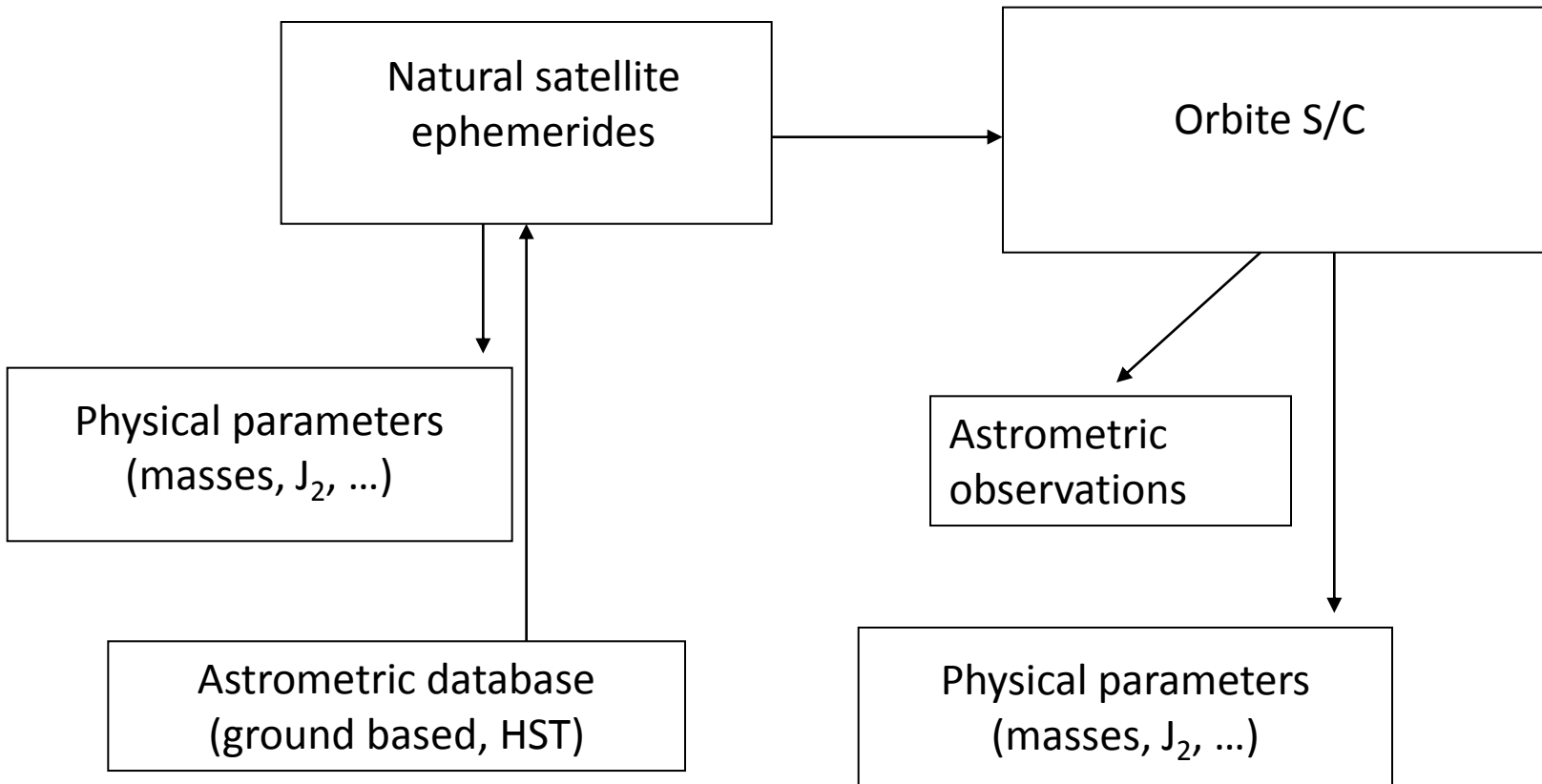
3- The ESPaCE network



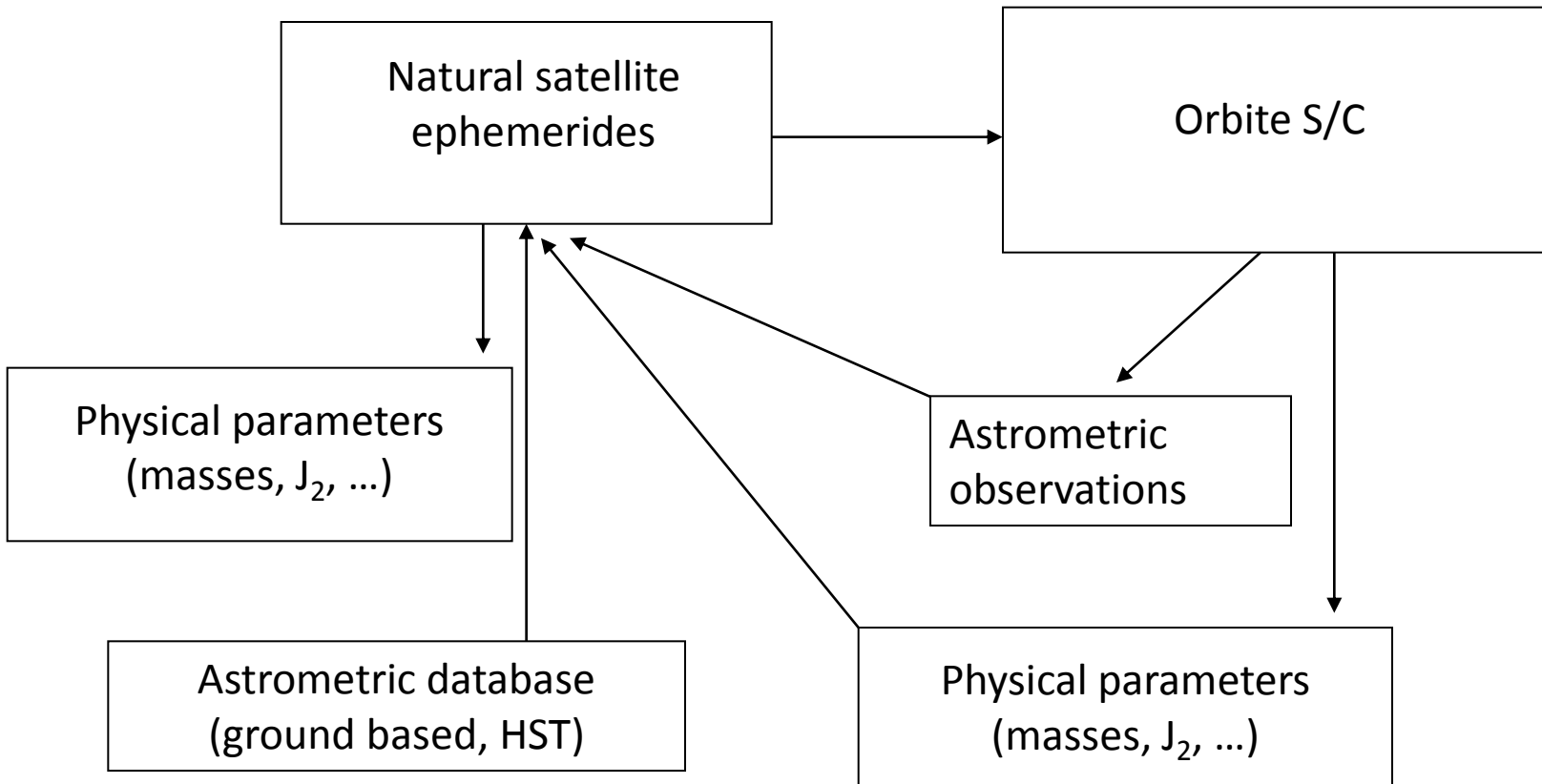
3- The ESPaCE network



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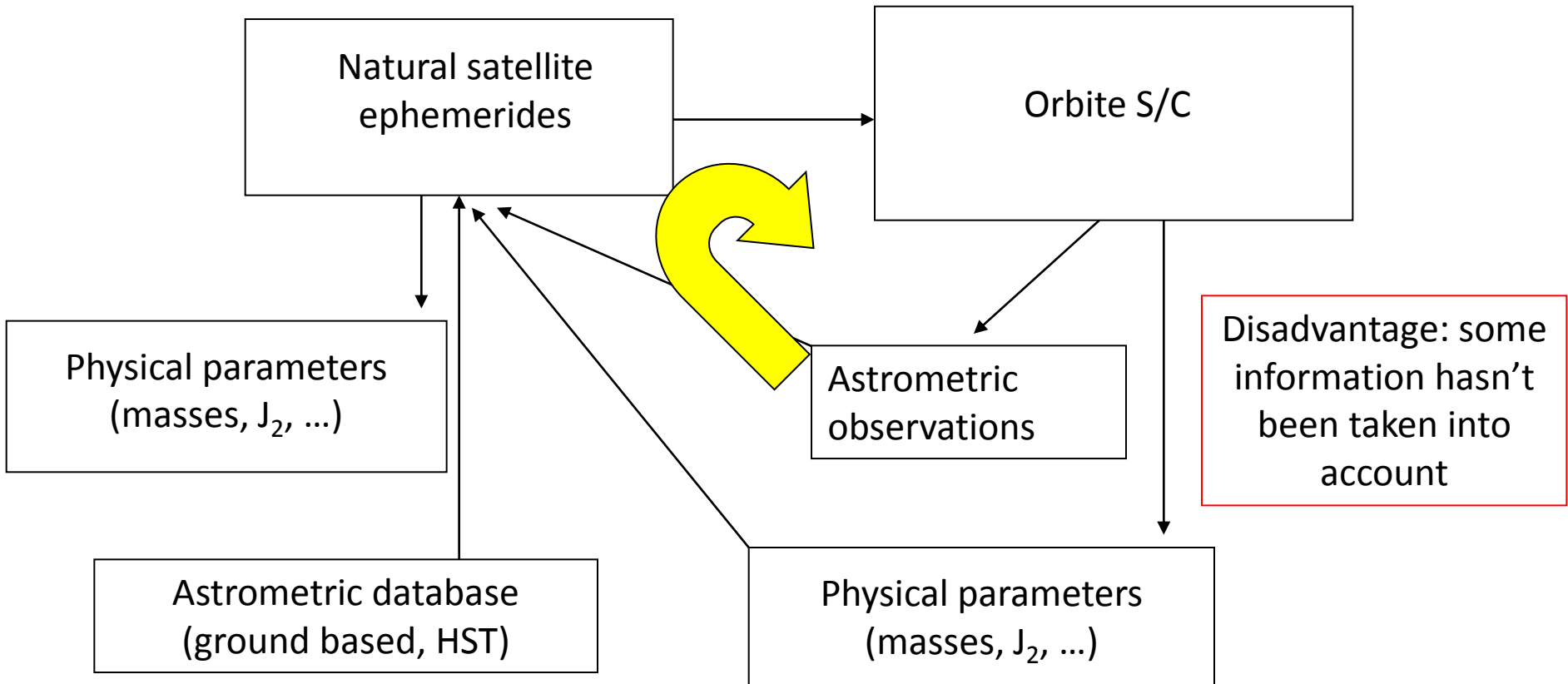


3- The ESPaCE network

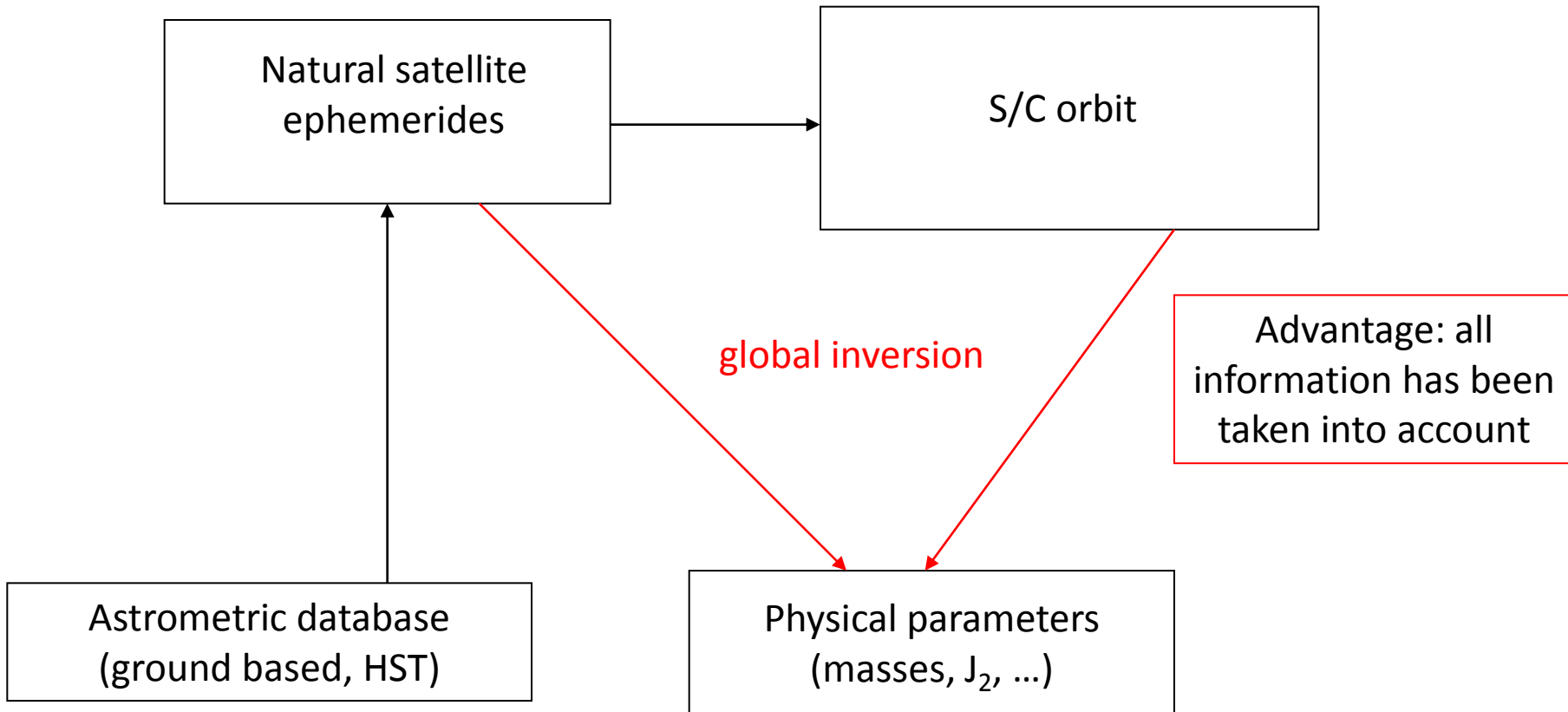


3- The ESPaCE network

Iterative method with independent fits

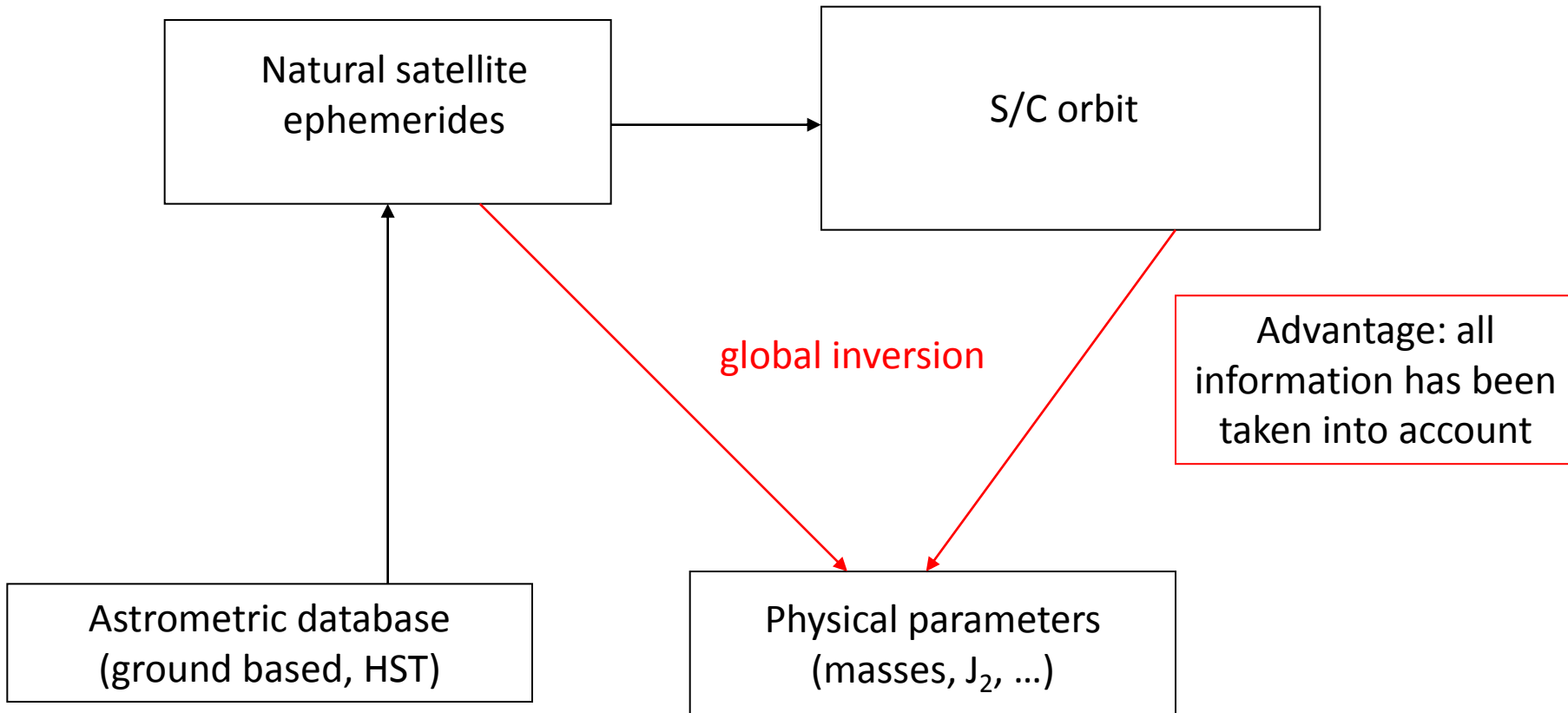


3- The ESPaCE network



3- The ESPaCE network

Method used only at JPL so far! (flyby of Miranda, flybys of Phobos...)



3- The ESPaCE network

An expertise rising in Europe: ESPACE (FP7) network (IMCCE, ROB, DLR, CNES, TUB, TUD, JIVE)

- Development of new orbit fitting techniques
- Production of HIGH accurate orbits for S/C and SAT
- Will help Europe to be at the US level in ephemeris developments
- Will be an important experience when treating next generation of European space mission (JUICE, ...)



Can SAT and S/C community get even closer?

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